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Freeze Vacuum Drying With Utilized Waste Heat of Condenser by Quick Drying Method

Awaludin Martin,^{a*} Utari Prayetno,^a Wandi Wahyudi,^a Iwan Kurniawan,^a and Romy,^a

^{a)} Conversion Energy Laboratory, Mechanical Engineering, Universitas Riau, Indonesia

*Corresponding author: awaludinmartin01@gmail.com

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ABSTRACT

Freeze vacuum drying process is an optimum process to dry the product without changing the physical and chemical properties of materials. The advantages of drying with freeze vacuum drying are can be maintain the structures, nutrient, and colors of original substances. A weakness of freeze vacuum drying is its high consumption of energy due to the long drying time required especially in the process of sublimation below triple point condition. The aim of this research are to optimizing freeze vacuum drying in order to reducing energy consumption by utilized waste heat of condenser to speed up the sublimation process and by using quick drying method. Thefreezing temperatures in this study were 6° C and 9° C with a variation of the drying time is 1, 2 and 4 hours. This research was result the water content losses in yam bean are 78% at a freeze temperature -9° C with drying time 4 hours.

KEY WORDS: Freeze Vacuum Drying; Drying Time; Yam Bean; Quick Drying.

1.0 INTRODUCTION

Freeze vacuum drying process is an optimum process to dry the product without changing the physical and chemical properties of materials [1]. The advantages of drying with freeze vacuum drying are; can be maintain the structures, nutrient, and colors of original substances [2,3 and 4]

Freeze-drying research has been done by previous researchers, among others; Drying aloe vera (aloevera) that contains a water content of 98.7% [1], tomatoes containing with water content of 93.4% [5], and pineapple with contains a water content of 85.30% [6].

A weakness of freeze vacuum drying is its high consumption of energy due to the long drying time required especially in the process of sublimation below triple point condition [7]. Drying time can be reduced by increasing temperature or decreasing pressure in the chamber (drying room).

Cuurently there are two problem in developing of freeze vacuum dryer; maintaining the quality of product and reducing energy consumption during vacuum freeze drying process. Acceleration of the sublimation process by utilizing waste heat of condenser is the one way to reducing energy consumption.

The aim of this research are to optimizing freeze vacuum drying in order to reducing energy consumption by utilized waste heat of condenser to speed up the sublimation process and by using quick drying method.

2.0 MATERIAL AND METHOD

2.1 Material

The material or fruit that used in this research is yam bean that has a water content of 85 to 90%.

2.2 Apparatus

Freeze vacuum drying with utilize waste heat of condenser has been designed and manufactured in the laboratory of conversion energy, Mechanical engineering, Universitas Riau. This freeze vacuum drying consists of a drying chamber with a capacity of 1 kg, refrigeration systems and heating systems from waste heat condenser. To measure the temperature, Thermocouple type K was used by using data acquisition Advantech Adam 4018. Initial and final mass of yam bean was measured by using digital weighing with accuracy of 0.1 gr.

1

Freeze vacuum drying was use a vacuum pump 1 HP with a flow rate 9 cubic feet per minute (CFM). This vacuum pump is uses to decreasing drying chamber pressure, so that the sublimation process can be done, schematic and freeze vacuum drying it can be seen in Figure 1 and 2.

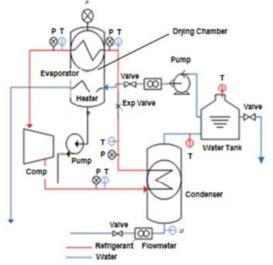


Figure 1: Scheme of freeze vacuum drying.

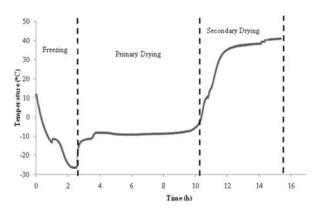
2.3 Experiment Procedures

To start the process, 50gr of yam bean that wet powder condition was input to drying chamber and then refrigeration system was turned on when the temperature of drying chamber is 20° C. The vacuum pump was then turned on when the material or yam bean temperatures reach to -6° C and -9° Cand appeared stable. And then, water that has been heated by using waste heat of condenser is flowed into the drying chamber for variation drying time is 1, 2 and 4 hours and the temperature of water was maintained in

40°C. After drying process in 1, 2 and 4 hour drying process was completed, the refrigeration system, vacuum pump and the flow of hot water was turned off. The water or the moisture content that loss in this process will be found by calculated the different weight before and after of drying process.



Figure 2: Apparatus of freeze vacuum drying.



The characteristics of the freeze vacuum drying process as the procedure mentioned above can be seen in figure 3 [1].



3.0 RESULT AND DISCUSSION

Freeze vacuum drying of yam bean has been done by quick drying method to determine the drying process characteristics on - 6° C and - 9° C by variation of drying time process is 1, 2 and 4 hour. From the testing with some variation, resulting different water losses in materials in different drying time. Wherethe largest water loss in the material is occurs in the process of drying for 4 hours at temperatures of 6° C and 9° C is 78 %.

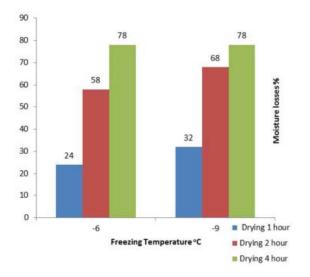


Figure 4: Comparison of water losses in different temperature and different drying time.

Figure 4 describes the comparison of the vacuum freeze drying yam bean in variation of drying time and drying temperature, its can be seen the water losses will be increase when the drying time is longer and the freeze temperature is lower. This is due to reach a lower freezing temperature takes a longer time, so that water that freezes in yam bean becomes more and then the amount of freezed water will be more to sublimated.

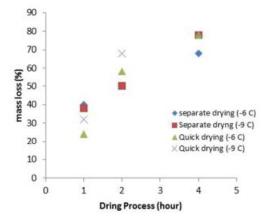


Figure 5: Comparison of Separate drying method and quick drying method.

In the previous research, vacuum freeze drying on yam bean has also been done by a separate drying method, and obtained the best drying results reached 84% within 6 hours of drying time [8]. Figure 5, shows a comparison the results of both drying methods and it can be seen in quick drying and separate drying method, the final result in 4 hour drying time is almost similar in drying temperature -6°C and -9°C. But in separate drying method where the drying temperature is -6°C the water losses of yam bean is lower than the other temperature, This condition indicates that the quick method is better than the separate methods bases on drying time process.

The process of freeze vacuum drying was described in Figure 6.Firstly the water in yam bean in liquid phase was freeze to drying temperature -6° C and -9° C become solid phase (process 1 - 2) or freezing process, after the water in solid phase the vacuum pump is turned on to decreasing pressure in drying chamber (process 2 - 3) or primary drying process, together with vacuum pump is turned on, water that has been heated by utilizing waste heat condenser flowed into the drying chamber (process 3 - 4) or secondary drying process.

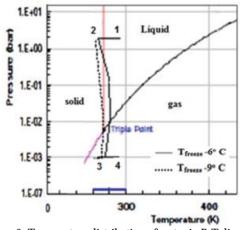


Figure 6: Temperature distribution of water in P-T diagram

Figure 6 show the trend line of distribution temperature in drying process at -6° C and -9° C with quick drying methods for4 hours. It can be seen in figure 6 that in temperature of material in -6° C, water in liquid phase was change to solid phase on freezing process but when the vacuum pump was turned on, the solid water was back to liquid phase and at the next process when the hot water was flowed into drying chamber the liquid water was evaporated, so that it can be concluded in this process there are not sublimation in the secondary drying process.

It can be seen also in figure 6 that in temperature of material in -9°C the process was complete. Water in liquid phase was change to solid phase on freezing process, when the vacuum pump was turned on, water in the solid phase is still on solid phase during primary drying process and when the hot water was flowed into drying chamber as a secondary drying process the water on solid phase was change to gas phase by sublimation.

The dried yam bean that dried by freeze vacuum drying in -9°C for4 hour can be seen in figure 7.



Figure 7: Dried yam bean.

4.0 CONCLUSIONS

Research of freeze vacuum drying with utilized waste heat of condenser by quick drying method was conducted at material temperature of -6° C and 9° C for 1, 2 and 4 hour and hot water from utilized waste heat of condenser was maintained at 40° C.

Water or moisture content losses maximum is 78% both at material temperature -6° C and 9° C for 4 hour, but on material temperature -6° C for 4 hour the freeze vacuum drying process is not complete because there are not the sublimation process at the secondary drying process.

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Carbon Footprint Estimation for Pole and Line Fishing Vessel According to Its Operation Mode -Study Case at Papua Fisheries-

Ede Mehta Wardhana, ^{a,*}, Trika Pitana,^b. and Ir. Suryanto,^c

^{a)}Postgraduate of Marine Engineering Student, Department of Marine Technology, Sepuluh Nopember Institute of Technology, Indonesia ^{b)}Lecturer at Postgraduate of Marine Engineering, Department of Marine Technology, Sepuluh Nopember Institute of Technology, Indonesia

^{c)}Ministry of Marine Affairs and Fisheries Republic of Indonesia

*Corresponding author: edewardhana@yahoo.com

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ABSTRACT

Carbon Footprint is one of the newest issue that people are concerned about especially on Fisheries business in Indonesia. The ships are growing bigger in terms of number and it makes the environment issue also became more concern for the people's life and wellbeing. In this experiment, those issues will be analyzed with Carbon Footprint on Fishing Ships in Sorong. This experiment will be analyzed using mathematical analysis based on literature that used in order to get the emission factor and also to calculate the carbon footprint emission on site. Those calculations will be used as basic logic calculation using the emission factor multiplied by fuel consumption. The purpose of this experiment is to understanding the Mode of the operation of the fishing ships in order to calculate the emissions. This experiment purpose is to get estimation of the amount of exhaust gas from fishing ships emission and also to get the constant value for each fuel that used for the fishing ships on the experiment site.

KEYWORDS: Carbon Footprint; Operational Model of the Fishing Ship; Emission Factor.

1.0 INTRODUCTION

1.1 Background

One of the biggest main causes of ocean pollution in Indonesia waterways is because there are so many fishing vessels who are operated in it. According to the report from the Ministry of Marine Affairs and Fisheries Republic of Indonesia on Number in 2011 [14], data about fishing vessel that registered is about 550.000. All these contemporary ships are very dependent on Fossil fuel for its propulsion, fishing catching activities and also to storage processing of those fish. Because of this dependent about fossil fuel, a certain problem is emerged. Not only a problem on Marine environment but also makes the price of fisheries who is very vulnerable to the price of the fluctuation from world fuel barrel price. [18]

In order to analyze the problem, it is important to do a measurement on fuel consumption on fishing vessel. There are at least 3 main reason to do those things [27], which are :

- 1. Environmental Sustainability : a Condition where the needs and supply for this generation (present condition) and future generation are accepted, without destroying or even slightly damaged the environment where the resource is. In other words, the place where the ships are set sail and operating can't disturb the availability of the resources because of the ships that operates in there.
- 2. Economic Sustainability : Many factors contributes to the economic value and economic ability on Fisheries sector. One of those things are ; Price Market, Investment, Labor price, price of transportation and the most important thing is the price of fossil fuel that's mainly used. The costs for fossil fuel could amount to 30 75 % from the production costs.

3. Competitive Advantage : If we can analyze and improve the energy consumption efficiency and the greenhouse gas effect, we could make a certain competitive advantage for our products. We could do these things using a demo and teach the fisherman and fisheries company about the improvement of environment security and availability. We could also tell the consumers about the advantage of choosing the fisheries product whose production process is very green and Eco-friendly

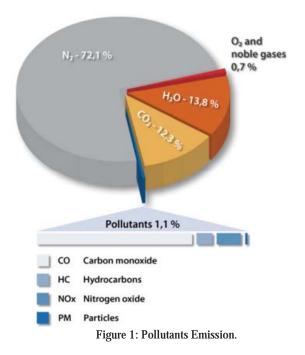
One of the efforts we're trying to ensure those availabilities is using the Ecolabelling on Fisheries Management. Ecolabelling is an instrument especially about based-market economic instrument with a purpose to direct consumer transaction behavior where they no longer oblivious and also take into consideration about other factor for consuming a product rather than just making a decision based on their market price [9]. The factors that we used for Ecolabelling are fair trade, support on micro scale fisheries production, environment and Ecology. One of the most famous fisheries organization in the world – FAO (Food and Agricultural Organization of United Nations) already do these Ecolabelling process on their fisheries product whereas the main point from this is to understand and to protect all potential fisheries resources. One of the fisheries product who have a bright potential is Tuna fish. For those product, there are many type of fishing vessel who specialize on catching and processing those. One of the Tuna fishing vessel is a Fishing vessel called Trawl, Purse Seine and Pole and Line. However since there are a new regulations from Indonesia government (Peraturan Menteri Kelautan Dan Perikanan Republik Indonesia Nomor 2/Permen-Kp/2015 - Tentang Larangan Penggunaan Alat Penangkapan Ikan Pukat Hela (Trawls) Dan Pukat Tarik (Seine Nets) Di Wilayah Pengelolaan Perikanan Negara Republik Indonesia) [16], who forbids a certain type of fishing vessel to operate within Indonesia waterways, currently the Pole and Line ships is the most dominant and mostly used to catch Tuna Fish. From those problem and explanation, it became clear that energy measurement is very important and we could analyze those things on one of the most needed vessel in Fisheries process, which is Pole and Line Type.

1.2 Literature Review

According to the book of *Emission Inventory Guide Book Group* 8 [7], Exhaust gas emission in Marine terms is all leftover emission that came from:

- Marine diesel engines who used as main propulsion and/or auxiliary engines
- Boiler who used as propulsion system for steam turbine
 gas turbines

From all the power unit that used in Ocean transportation industries, Marine Diesel Engine is the most dominant for main propulsion[4]. All those engines are using a certain type of fossil fuel in order to operate, which resulted on a certain Emission Factor for each engine. All exhaust gas emission from Marine Diesel contains Nitrogen, Oxygen, Carbon Dioxide and Water Vapour and also Sulfur. Other than those there are also Hydrocarbon and Particulate Material, Metal and Organic micropollutants that cannot be re-used. The comparison between



those pollutants could be seen on the figure 1:

All those exhaust emission who has a negative effect on environment (greenhouse gas effect) are named Carbon Footprint [10]. Carbon Footprint is measured all the total of greenhouse gas whether it is direct or indirect who produced by a certain type of activities. or those things could also came from the accumulation from a certain production process [27]. Carbon footprint could be divided by 2 types which are Primary Carbon Footprint and Secondary Carbon Footprint. Primary carbon footprint is an emission who came directly from combustion of the fossil fuel, while secondary carbon footprint is the CO₂ emission who came indirectly [10]. The example of secondary carbon footprint is the electricity consumption. All the research from the expert creates a certain facts that there is an escalation of the amount of CO2 at the atmosphere which could be passed the limit. Every day the amount and the concentrates of CO2 is increasing and it has a correlation between those increase and High activities from the people on Earth. In Marine world itself, the combustion process from the Main Engine is one of the main reasons of Primary Carbon Footprint. In order to solve this problem, an approach based on Consumption behavior could supply an approach based on production that invented by Gas Rumah Kaca Nasional Organization and also agreed on Kyoto Protocol [17]. Carbon Footprint with consumption based could facilitate International Cooperation between developing country and developed country. Other than those purposes, the approach also could make the consumer realize how much greenhouse gas emission that they make because of their lifestyle and indirectly it makes them aware about the emission problems. Carbon footprint usually told not with unit based on territory, but it is measured by unit of mass (kg, ton, etc).

Regulation about the limitation of the emission, specifically about SO2 and NOx is regulated by IMO (International Maritime Organization). NOx emission from the main engines have a limitation for the diesel engines with power more than 130 kW, and for those types here are the limitation values [8]:

$$\begin{array}{c} 17 \ g/kWh \ when \ n < 130 \\ 45 \ x \ n^{-0.2} \ g/kWh \ when \ 130 < n < 2000 \\ 9.84 \ g/kWh \ when \ n > 2000 \end{array}$$

For the estimation of emission calculation, there are a few methods that we can be used. However from all those method, the most basic method to calculate the exhaust gas emission is shown in the equation (1):

Emission = Fuel sold x Emission factor(1)

Where the value of Fuel sold could be separated into two parts which are Residual Bunker Fuel Oil or more common known as Heavy Fuel Oil (HFO) and Distillate Fuel or more commonly known as Marine Diesel Oil (MDO) even though that for certain country there are another type of fuel that they're using on. In Practice, every ships have its own specification, engine power, speed and gross tonnage according to each function.

1.3 Purpose of Study

Because of new regulations from Indonesia government for Fishing vessel that could operate, the growth of shipping activity and more exploitation on marine resources, and also the limitation for exhaust gas emission both from IMO and from government itself (Peraturan Menteri Lingkungan Hidup Republik Indonesia Nomor 7 Tahun 2014 Tentang Kerugian Lingkungan Hidup Akibat Pencemaran Dan/Atau Kerusakan Lingkungan Hidup) [13], it resulted in a certain unanswered scientific questions. Those questions are how the Operation Mode from the fishing vessel when they're about to catch the fish? How it will affect the emission? How much for the estimation of exhaust gas for fishing vessel that came from Main Engine? And how is the ratio between exhaust gas emission estimation value with Fisheries production estimation?

The purpose of this paper is to obtain the detailed data and information about the Operation Mode from fishing Vessel, Fuel oil consumption, the value of ship emission who could take effect on marine environment, and also to obtain the constant value and also the method to calculate Carbon Footprint on Fishing Vessel. With all these obtained information, it's expected to help the authority of Indonesia Government work better, especially on The Ministry of Marine Affairs and Fisheries of Republic Indonesia which resulted as a reference for alternate policy to get the business of fish catching (especially on Tuna Cakalang Tongkol – TCT Production) more Eco-friendly, low fuel oil consumption, and low CO according to the goal from Indonesia Government Program

1.4 Research Location

The Location for this research is at Waterways on Sorong region. For Fishing Port is located on Cakalang (Kuda Laut)Sorong, Desa Kampung Baru, Kec. Sorong Barat. This port has 2 docks, revetment and open drainage in order to facilitate the fisherman to do catching activities. This port is quite closed to the Sorong central activities. This port also manage and supervise other location such as : Kota Sorong, Kabupaten Sorong, Kabupaten Raja Ampat, Kabupaten Sorong Selatan, Kabupaten Maybrat, Kabupaten Tambrauw, Kabupaten Bintuni/Wimro.

The data obtained from Pelabuhan Indonesia IV Office Branch is told that the wind speed is on 7 knot/hour on September and December. While the data about the tidal is :

- High high Water Spring (HWS) : 1,50 m LWS
- Low Low Water Spring (LWS) : 1,00 m LWS.

From each month there are fluctuation on wave height because it's all depends on the season which is influence the wind blows. The wave on site could go up to 3 meter depends on what season it'll be. The location of this research could be seen in Figure 2 and Figure 3 for the docks at the fishing port :



Figure 2: Sorong Region



Figure 3: One of the docks from Fishing Port at Sorong

For the fishing season division, usually it is associated with the sea breeze or onshore breeze in the location. The peak season usually start in October until April (Musim angin barat), and for the transition (not so much fish to catch) is on May until August (Musim angin timur). In the transition season, all the catching effort and activites will be decreased drastically. Detail about the season of fish catching is shown in the figure 4:

Waktu tangkap		Puncak			Paceklik			Sedang					
	Bulan	Sep	Okt	Nov	Des	Dan	Feb	Mar	Apr	Mei	Jun	Jul	Ags
Musim angin		Barat			Peralihan	1		Timur		Peral	itan 2		

Figure 4: Graph of fishing ships season on Pole and Line Vessel

2.0 METHODOLOGY

2.1. Framework and Data Collection

Exhaust gas emission frol the fishing vessel is very dependent on what type of operation from those ships in a certain region. In this paper, the sample is obtained when the fishing vessel with pole and line type is point the catching activities in Sorong waterways. According to the data of location geography, here is the figure on the maps of catching activities as shown in figure 5:



Figure 5: Catching Activities

During the process for catching the fish, we could obtain these data in order for the next analysis:

- RPM Engine
- Time of Sailing
- Process and activities that's been doing / Operation Mode
- Longitude Latitude
- Fuel Oil consumption on certain activities at certain time of sailing.

2.2. Fuel Oil Consumption and Emission Factor

In the exhaust gas emission calculation, we need to understand and obtain the data about the amount of fuel oil that used for the activities. According to the data observation from the fish catching activity, we obtained the amount of fuel oil consumption in a certain Operation Mode that can be seen in the table 1:

Table	1:	Fuel	Oil	Consumption

Used Engine	Fuel Oil Consumption (Ltr:Day)	Operation Mode
	143.52	Warm Up
	1348.94	Goes to Quay
Main Engine 330 PK	1119.29	Goes to Fishing Ground
	463.05	at Fishing Ground
	312.59	Back to the Docks.

According from those data, for the next step we could estimate the emission value. However in order to know the exact value we also need the data about the emission factor for an emission. The value from those emission factors are obtained and shown in the table 2 down below:

		Table 2	2: CO	$_2 \mathrm{Em}$	issi	on F	acto	r			
Fish	NOx	\$O2	CO2	HC	PM	sfc	No	\$0 2	CO2	HC	P M
Catching		22 - 03	in g/kWb	į				in l	g/tonne	fuel	
At Sea	13.9	11.5	685	0.5		215	65	53	3179	1.9	
In Port	13.4	12.2	722	0.4	0.5	227	59	54	3179	1.5	3.6
Manouvering	13	12.2	725	0.6	1.1	225	57	54	3179	2.6	4.6
	NOx	\$02	CO2	HC	PM						
Fish Catching	Kg/To n	Kg/Ton	Kg/TJ	Kg /To n	Kg /To n						
At Sea	11	19	74100	26	2.4						
In Port	10.5	20	74100	24	2.4						
Manouvering	10.1	20	74100	28	3.4						

2.3. Emission Calculation

Method that is used for the analysis of the estimation of fishing vessel emission is based on observation of fuel oil consumption from fish catching activity. Based on those results, we compare the result with Methodological standard of Europe where these standard already adopted on a research conducted by oleh Carlo Trozzi and Rita Vaccaro in their paper: Methodologies for Estimating Air Pollutant Emissions from Ships [26]. These researches are executed on Uni-Europa region with a purpose to obtain the method to estimate fuel oil consumption and also its emission value using the statistic for each ship traffic in European region. The type of the pollution that is used and analyze in those research is the pollution from combustion process. In those papers, the author combine twelve type of ships where the data of emission factor, type of engine, shipping conditions and fuel oil consumption is obtained. That standard is finally called as the **MEET Framework standard**

For the emission calculation method using MEET Framework standard, here is the formula that used for the calculation as shown in equation (2) for Total Emission and equation (3) for Total Emission from a certain type of pollutant, fuel oil, ships and engine:

$$E_i = \sum jkl \ E_{ijkl} \tag{2}$$

Where :

$$E_{iikl} = S_{ik} (GT) x t_{ikl} x F_{iil}$$
(3)

Where :

Ei = Total Emission from a certain pollutant

Eijkl = Total Emission from a certain pollutant who came from using a certain type of fuel oil, on a certain class of ships and also a certain type of engine.

 Σjkl = where; i = pollutant, j = fuel, k = class of ship for consumption class, l = class type engine for emission factor characteristics,

Sjk (GT) = Fuel oil consumption in a certain class of ships (Units in Gross Tonnage)

tjkl = amount of days for ships navigation on a certain class

of ships that used certain type of engine and also certain type of fuel oil

Fijl = Emission factor from a certain pollutant on a certain fuel that came from a certain type of

However, one of the weaknesses from this equation is inability to project the result on a real time and according to its real condition. In order to obtain the result as close to the real condition in practice, we need more detailed methodology that needs several more data:

- Navigation statistics, also the data from ships gross tonnage and the type of fuel that is used and also the mean time of consumption, who are distributed according to the ships class.
- Statistics of the movement of the ships in order to obtain the detailed mission estimation. Or we could use :
- Ships distribution and general statistics of ships movement in order to get the emission estimation.

From those information, we could obtain a number of days from a different ships operation mode. From those data, we finally could obtain the more detailed emission calculation formula as shown in equation (4) and equation (5):

$$E_i = \sum jklm \ E_{ijkl} \tag{4}$$

where :

$$E_{ijklm} = S_{jkm} (GT) x t_{jklm} x F_{ijlm}$$
(5)

3.0 RESULT AND DISCUSSIONS

3.1. Exhaust Gas Emission Calculation

From the research that we are conducting, we get the result of fuel oil consumption in Table. 1. From those researches, we obtained the value of the Fuel Sold that we needed for the Formula 1. The next thing we are doing is multiply those values with the emission factor in Table 2. And from those calculations, we get the result. Table 3 is for the result of emission of CO_2 per trip:

Table 3:	Result	of	Emission o	of CO ₂	Per Trip)

Used Engine	Fuel Oil Consumption (KI)	Calorific Value (TJ/Kl)	Operation Mode	Emission Factor (Kg/TJ)	Emission CO ₂ (Kg)
	0,143	0,000036	Warm Up	74100	0,2753
	0,463	0,000036	Goes to Quay	74100	3,6077
Main Engine	1,119	0,000036	Goes to Fishing Ground	74100	2,9276
330 HP	0,312	0,000036	Fishing Ground	74100	1,2981
	1,348	0,000036	Back to the Docks	74100	0,8339
Total	3,38			Total	8,9425

Table 4 is for the result of emission of NOx per trip as shown in table below:

Table 4: Result of Emission NOx Per Trip

Used Engine	Fuel Oil Consumption (Kl)	Operation Mode	Emission Factor (Kg/Ton)	Emission NOx (Kg)
	0,143	Warm Up	10,5	1,2646
	0,463	Goes to Quay	11	12,0354
Main Engine	1,119	Goes to Fishing Ground	11	10,0475
330 HP	0,312	Fishing Ground	10,1	4,3455
	1,348	Back to the Docks	11	2,8883
Tota1	3,38		Total	30,5813

For the result of emission on SO₂ per trip, it is shown on Table 5

Used Engine	Fuel Oil Consumption (Kl)	Operation Mode	Emission Factor (Kg/Ton)	Emission SO ₂ (Kg)
	0,143	Warm Up	20	1,9192
	0,463	Goes to Quay	19	21,0393
Main Engine	1,119	Goes to Fishing Ground	19	17,5695
330 HP	0,312	Fishing Ground	20	8,0423
	1,348	Back to the Docks	19	4,9889
Tota1	3,38		Tota1	53,5591

For the result of emission on the emission of Hidrocarbon (HC) per trip, it is shown on Table 6 :

Used Engine	Fuel Oil Consumption (Kl)	Operation Mode	Emission Factor (Kg/Ton)	Emission HC (Kg)
	0,143	Warm Up	24	2,3992
	0,463	Goes to Quay	26	28,2882
Main Engine	1,119	Goes to Fishing Ground	26	23,8832
330 HP	0,312	Fishing Ground	28	10,2015
	1,348	Back to the Docks	26	6,8270
Tota1	3,38		Tota1	71,5990

Table 6: Result of Emission HC Per Trip

For the result of emission on the emission of Particulate Matter (PM) per trip, it is shown on Table 7 :

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Used Engine	Fuel Oil Consumption (Kl)	Operation Mode	Emission Factor (Kg/Ton)	Emission PM (Kg)
	0,143	Warm Up	2.4	0,2428
	0,463	Goes to Quay	2.4	2,6789
Main Engine	1,119	Goes to Fishing Ground	2.4	2,2504
330 HP	0,312	Fishing Ground	3.4	1,0126
	1,348	Back to the Docks	2.4	0,6302
Tota1	3,38		Total	6,8148

And for the emission calculation of CO is shown on Table 8 :

		Sull of Emission		
Used Engine	Fuel Oil Consumption (Kl)	Operation Mode	Emission Factor (Kg/Ton)	Emission PM (Kg)
	0,143	Warm Up	140	
	0,463	Goes to Quay	43.5	39,9554
Main Engine	1,119	Goes to Fishing Ground	43.5	35,6912
330 HP	0,312	Fishing Ground	-	-
	1,348	Back to the Docks	43.5	11,4220
Tota1	3,38		Total	87,0686

Table 8: Result of Emission CO Per Trip

From all those data, we could conclude it and find the whole total emission that occured and it shown on Table 9 :

Table 9: Result of Total Emission

Moda	TotalCO2 (Kg)	NOx	SO 2	нс	PM	со
Warm Up	0,2753	1,26	1,91	2,39	0,24	-
Goes to Quay	3,6077	12,03	21,03	28,28	2,67	39,95
Goes to Fishing Ground	2,9276	10,04	17,56	23,88	2,25	35,65
Fishing Ground	1,2981	4,34	8,04	10,20	1,01	-
Back to the Docks	0,8339	2,88	4,98	6,82	0,63	11,42
Total (Kg)	8,9425	30,58	53,55	71,59	6,81	87,06
Total Emission (Kg)	258,56					
Total Emission 4 Ships	1034,26					
Annual Total Emission (20 Trip)	20685,23					
Total Emission (Ton)	20,68					

3.2. Method Comparison

In order to find the margin defisit between the experiment result and the MEET Framework, we can compare the result of exhaust gas emission using both method to calculate it and find the deficit margin. However, before we can calculate the result of the Carbon Footprint, we need another data which is the sample Fish Product Production for Pole and Line at Sorong. Data about monthly production for Pole and Line ships at Sorong region is shown from the figure 6:

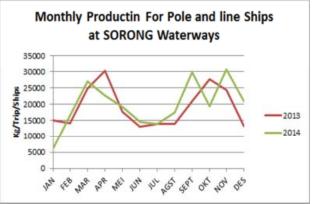


Figure 6: Graph of Pole and Line Ships Production at Sorong

The data about calculation result and comparison method for exhaust gas emission with fisheries production could be seen in these graphs. on figure 7 it is shown the graph of CO_2 Carbon Footprint:

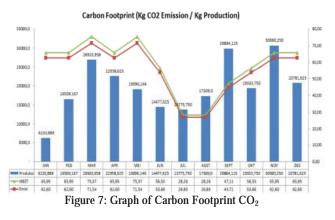
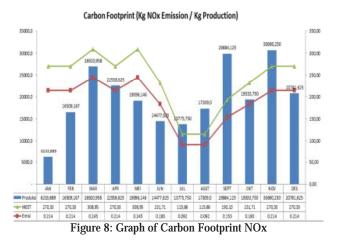
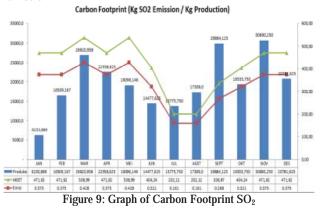


Figure 8 is for the result of Carbon Emission NOx :

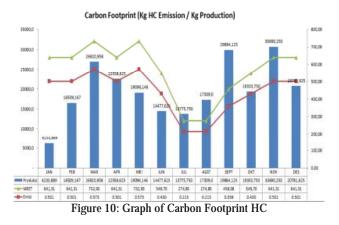


On Figure 9, is shown the graph of carbon footprint of SO₂

emission



For the result of carbon footprint on Hidrocarbon (HC) emission, it is shown on Figure 10 :



For the result of carbon footprint on of Particulate Matter (PM) emission, it is shown on Figure 11 :



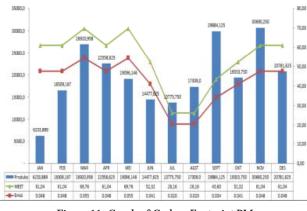
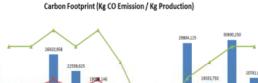
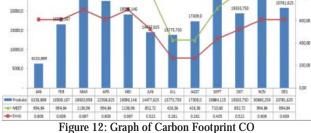


Figure 11: Graph of Carbon Footprint PM

And for the result of carbon footprint on of CO emission, it is shown on Figure 12 :





And for the margin deficit between the experiment calcualtion and MEET Framework calculation is shown in the table 9:

Table 9: Percentage different

Percentage of Comparison					
CO2	NOx	\$O2	HC	PM	8
3%	12%	11%	12%	12%	24%

3.3. Rules and Regulation

15000.0

According to the regulation from the Ministry for the Environment (Peraturan Menteri Lingkungan Hidup Republik Indonesia Nomor 7 Tahun 2014 Tentang Kerugian Lingkungan Hidup Akibat Pencemaran Dan/Atau Kerusakan Lingkungan Hidup) [13] stated that there are the limit value for each air pollution for each polluting unit. According to the accumulation of each polluting unit value and also takes into consideration about the diversity of the industries with the different type and parameter of pollution unit, we could calculate the damage of the environment based on single unit of contaminant / pollution for each parameter.

The air or gas emission parameter or even liquid waste parameter that used to calculate the pollution for each value of contaminant is shown in the Table 10:

 Table 10: Pollution Unit Values for Various Parameters Air

 Emissions / Gas

Parameter	Air Pollution Index
NON LOGAM :	
Ammonia (NH3)	350 g
Chlorin (Cl2)	7 Kg
Hidrogen Chlorida (HCl)	4 Kg
Hidrogen Fluorida (HF)	7 Kg
Carbon Monoksida (CO)	400 Kg
Nitrogen Oksida (NOx)	200 Kg
Sulfur Oksida (SOx)	200 Kg
Batubara (Coal)	250 Kg
Minyak (Oil)	150 Kg
Semen (Cement)	100 Kg
Particulate Matter	250 Kg
Total Sulfur Tereduksi (H2S)	25 Kg
Metal :	
Arsenic (As)	4 g
Antimony (Sb)	10 g
Cadmium (Cd)	10 g
Lead (Pb)	10 g
Mercury (Hg)	4 g
Zinc (Zn)	40 g

These are the result between each method that are used with the rules and regulations from Indonesia Government and it is shown on the Table 11:

Table 11:	Compliance	with Rules	and Reg	ulations

Parameter	Air Pollution Index	Using Calculation From Experiment		MEET Framework Calculation		Acc/No
NON METAL :				0		201
Ammonia (NH3)	350 g					
Chlorin (Cl2)	7 Kg					
Hidrogen Chlorida (HCI)	4 Kg					
Hidrogen Fluorida (HF)	7 Kg]				
Carbon Monoksida (CO)	400 Kg	87,07	Kg	142,12	Kg	Accepted
Nitrogen Oksida (NOx)	200 Kg	30,58	Kg	38,62	Kg	Accepted
Sulfur Oksida (SO2)	200 Kg	53,56	Kg	67,37	Kg	Accepted
Batubara (Coal)	250 Kg					
Minyak (Oil)	150 Kg	1				
Semen (Cement)	100 Kg	1				
Particulate Matter	250 Kg	6,81	Kg	8,72	Kg	Accepted
Total Sulfur Tereduksi (H2S)	25 Kg					
METAL :						
Arsenic (As)	4 g	1				
Antimony (Sb)	10 g					
Cadmium (Cd)	10 g]				
Lead (Pb)	10 g]				
Mercury (Hg)	4 g					
Zinc (Zn)	40 g	1				

4.0 CONCLUSION

Sorong region as one of the most common place for Papua region fisheries activities have so much ships. All thoses ships mainly uses Diesel Engine and certain fuel oil and therefore they produce a lot of emission. Those thing will influenced the Eco-Labelling that's planned to do in Indonesia fisheries. In this research we try to give an explanation how big for the influences for a certain type of fishing ships (pole and line) can contribute to the pollution at sea. From this research is is foundtThere are 5 things / 5 activities on Operation Mode of Pole and Line fishing ships in Indonesia region, those things are Goes to Quay, Goes to Fishing Ground, at Fishing Ground, and Back to the Docks. All this five operation mode is obtained based on survey by Kementrian Kelautan dan Perikanan in Indonesia waterways.

All those five operation mode also have the different CO_2 emission value, which are :

Warm Up	: 0,27 Kg
Coos to Ouov	. 26

Goes to Quay : 3,60 Kg Goes to Fishing Ground : 2,92 Kg

• at Fishing Ground : 1,29 Kg

Back to the Docks : 0,83 Kg

These could happen because the fuel oil consumption and emission factor is different for each operation load which resulted in a different value of exhaust gas emissions.

The result of total exhaust gas emission also has different value between the experimental one and MEET Framework standard. The percentage deficit is approximately on 3% to 12 % based on the type of the emission. That result is because there are simplification on MEET Framework where they only assuming the fuel consumption based on ships gross tonnage. Other than those, the amount of day for ships at a certain operation mode is also have a huge contribution between mismatch on the calculation and in practices. However, based on the calculation all the types of emission is below the limit from the regulations of Indonesia Government and Authority

From all of those calculations, we could also conclude that each year Pole and Line ships could do a trip until 20 times and also could obtain:

179 Kg CO₂ emission / 61.260 Kg Fish

For each CO2 emission that resulted form combustion process of Pole and Line ships is resulted on the productions of fisheries:

• 29 g Emisi CO₂ / 1 Kg Fish

These results are shown to us that the catching process using Pole and Line type of the Fishing Vessel is one of the catching tools who is very Eco-Friendly compared to the other type of the fishing vessels like Trawl and Purse Seine and the emission resulted from Pole and Line catching activity is one of the lowest in all of the fishing vessel.

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Finite Element Analysis of Wood Structural Joints on Traditional Wooden Ship

Yohanes, ^{a,*} Musthafa Akbar ^a and Reysca Admi Aksa ^a

^{a)}Mechanical Engineering, Universitas Riau, Indonesia

*Corresponding author: yohanes_tmesin@yahoo.com

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ABSTRACT

Traditional ship often made by woods materials and it was made without proper engineering procedure. This research focuses on a case study in Bagan Siapiapi, Riau Province, Indonesia where a large wooden ship was manufactured. One of the sources of material failure in the manufacturing of wooden ship is located at the joint. In this research, a modification of joint design has been studied where 4 design model have been offered by using glue as the attachment materials and 5 other design by using bolt as the connection method. A finite element method was used to study the strength of the joint which has been guided by a standard issued by Indonesian Classification Bureau. There are 9 design of joints were modeled and studied which have been varied using two different wooden materials such as 'keruing' and 'meranti'. A uniform loading was applied on all models and materials. The applied loadings are buoyancy force, gravity force, and pre-stress loading at the bolt. The result from simulation generates a stresscontour indicating the stress level on the materials. It was concluded that the model of connection hooked straight lip which is connected with 4 pieces M14 bolts with wood material keruing a recommended model for traditional wooden boat building. This design gives 1.605 mm deformation with maximum stress of 217.51 MPa.

KEY WORDS: Traditional Ship, wood joints, finite element method.

NOMENCLATURE

 $\begin{array}{lll} \rho & \mbox{Density of fluid} \\ V_{ter} & \mbox{Volume of submerged part} \\ F_{apung} & \mbox{Bouyancy load} \\ g & \mbox{Gravitational force} \end{array}$

1.0 INTRODUCTION

Bagan Siapiapi has been known as the biggest wooden ship manufacturer in Indonesia. Ship produced in this region has been used not only in Indonesia but also outside Indonesia. The ship was used by fisherman to catch the fish. Manufacturing of this wooden ship is still undergoing by conventional and traditional method without any proper engineering procedure. It is often that the ship was made through series knowledge passed by one generation to the other generation. Therefore, there is no standard in the manufacturing of a wooden ship.

Series effort to improve the design of the wooden ship in Bagan Siapiapi has been started by Damanik [1] in 2004. In his research, determination of center of gravity and estimation of ship's loading have been studied. It has been recommended that there is a need for further study in the subject of determination of critical point in the joint based on stress analysis. Stress analysis is an important parameter in the design of ship structure. The analysis and the manufacturing of wooden ship are still conducted based on a proper engineering procedure and standard. However there is a lack of research in the wooden ship.

Stress in the ship structure are often comes from a nonuniform loading due to sea wave. There is a loading combination between hydrostatic and hydrodynamic loads and it will results in bending moment and shear stress at the joint. Therefore, the joint should be designed carefully because at this point the loading becomes critical. In order to obtain the maximum stress at the ship structure, an experimental method or numerical method can be used to investigate the particular stress.

This purpose of this research is to develop several designs of joints at the wooden structure applied to the traditional wooden ship. The analysis was conducted based on numerical methods which use a finite element method to investigate the resulting stress. The expected results are the recommended design of joint and the optimum joint design which gives a high strength with minimum geometry.

2.0 METHODOLOGY

Joint area is the weakest point in the ship structure and responsible for the most of structural failure in the ship structure. There are two methods to connect the structure. The first one is using glue while the other method is using bolt. As for the joint in the wooden ship structure, the reference is based on [3] while the standard for experimental of wooden structure is based on the Indonesia classification bureau.

2.1 Design of Wood Joints using Bolt

The choice of bolts in the wooden joint is based on the thickness of the wooden structure. According to Indonesia classification bureau, for 110 mm of thickness, the choice of bolt is M14. The number of bolt to be used is chosen based on width of the joint which is 230 mm. Therefore the number of bolts to be used is 4. The position of the bolts is also regulated in the standard of Indonesia classification bureau as shown in Table 1.

Table 1: Position the mounting bolts based on standards BKI [4]

Edge cut with a hand	Edge cut with machines	Edge profile does not result snippet
1,75d _b	1,50d _b	1,25d _b

Thus, the calculation results be obtained as follows:

- a. Distance to the edge of the bolt (S1) = $1.75 \times 14 \text{ mm} = 24.5 \text{ mm}$
- b. Distance to the edge of the bolt unencumbered (S2) = Distance to edge bolt (S1) = 24.5 mm
- c. The distance between the bolt (S) = 275 mm (24.5 (2) + 14 mm) = 212 mm

Based on the design parameters of the above, it can be made a model joint design of timber ships Siapiapi chart, shown in Figure 1 to Figure 5.

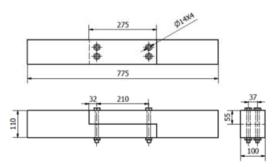


Figure 1: Design of Straight Lip Joint with Bolt (B1)

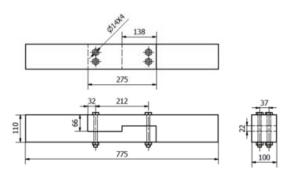


Figure 2: Design of Hook Straight Lip Joint with Bolt (B2)

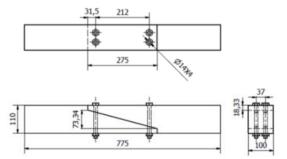


Figure 3: Design of Oblique Lip Joint with Bolt (B3)

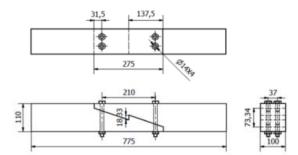


Figure 4: Design of Hook Oblique Lip Joint with Bolt (B4)

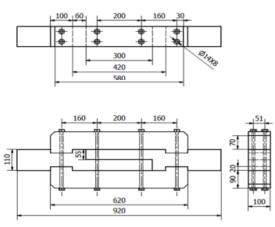


Figure 5: Design of Key Pinch Joint (B5)

15

2.2 Design of Wood Joints using Glue

According to standard of Indonesia classification bureau, at the joint connected by glue, the required thickness must be less than 1 over ten of the height, but must not less than 5 mm and not more than 20 mm. The requirements for the experiment on the joint connected by glue are:

- a. Experimental subject must be from the part connected by the glue.
- b. The part connected by the glue must have addition length around 150 mm.
- c. The experiment must be conducted at least 10% from 'gading-gading', deck beams and all important element of strength longitude.
- d. The specimen should not be given the ultimate handling in excess of that provided at the actual construction.

According the above requirements, thus the development of design for the gading-gading joint on the wooden ship can be presented in Figure 6 to Figure 9.

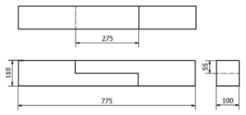


Figure 6: Design of Straight Lip Joint (L1)





Figure 7: Design of Hook Lip Joint (L2)



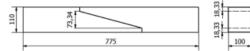


Figure 8: Design of Oblique Lip Joint (L3)

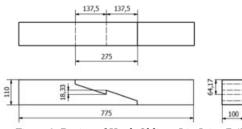


Figure 9: Design of Hook Oblique Lip Joint (L4)

2.3 Finite Element Method

2.3.1 Loading Conditions

The loading on the wooden ship is limited to the external loading, which is the loads due to buoyancy force and the loads due to its own weight. The buoyancy force is obtained based on the volume of the wooden ship, density of the fluid, and also based on the gravity force. The volume is determined based on the previous research, which was defined as the total mass of the wooden ship divided by the density of the fluid. The total mass of the wooden ship is 6308.04 kg [1]. Therefore, the volume can be found by using the following equations.

$$V_{submerged} = \frac{Mass of Ship}{\rho_{fluids}}$$
$$V_{submerged} = \frac{6308,04 \ kg}{1012 \ kg/m^3}$$
$$V_{submerged} = 6,15 \ m^3$$

Using the above equation, the buoyant force is obtained:

 $F_{floatable} = \rho_{sea water} x g x V_{submarget}$ $F_{floatable} = 1025 kg/m^3 x 9,18 m/s^2 x 6,15 m^3$ $F_{floatable} = 61.839,7875 Newton$

2.3.2 Meshing Strategy

The meshing strategy applied in this research is based on the coarse type or default. This meshing strategy can be used for the general cases but not for the contact part where it needs refinement mesh. The refinement mesh can be seen at the bolts as show in Figure 10 to Figure 12.

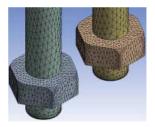


Figure 10: Refinement on Bolt



Figure 11: Meshing on the connection bolt with refinement on the contact between the joint with the bolt

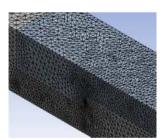


Figure 12: Refinement mesh in the contact area connection

2.2.3 Material Model

The materials studied in this research are keruing and meranti. The mechanical properties of these wooden materials can be seen in Table 2 and Table 3. Only 9 mechanical properties are required in the analysis [6]. The ratio of fiber orientation for the elasticity modulus and shear modulus are based on the previous study [7].

Table 2: Mechani	ical properties	of Keruing Wood
------------------	-----------------	-----------------

No	Parameter	Axis	Value
1	Elastic Modulus	х	15000 MPa
2		у	10000 MPa
3		Z	833,33 MPa
4	Shear Modulus	xy	1379 MPa
5		yz	114,91 MPa
6		XZ	91,33MPa
7	Poisson Ratio	Х	0,33
8		у	0,33
9		Z	0,33
10	Density		780 Kg/m ³

No	Parameter	Axis	Value
1	Elastic Modulus	х	13900 MPa
2		у	9266,6 MPa
3		Z	772,22 MPa
4	Shear Modulus	ху	1379 MPa
5		yz	114,91 MPa
6		XZ	91,33 MPa
7	Poisson Ratio	х	0,33
8		у	0,33
9		Z	0,33
10	Density		865 Kg/m ³

The material for bolts is steel material and its mechanical properties can be found in Table 4.

Table 4: Mechanical properties of structural steel			
Densitas	7850	Kg/m ³	
Elastic Modulus	200	GPa	
Poisson's ratio	0,3		
Bulk Modulus	166,7	GPa	
Shear Modulus	76,9	GPa	
Yield Strength	250	MPa	
Ultimate Tensile Strength	460	MPa	

2.2.4 Boundary Conditions

The boundary conditions are necessary for the inclusion of rigid body motion [8]. The axis definition on the model of Bagan Siapiapi traditional wooden ship can be found in Figure 13. At the joint connected by glue, the applied load is based on the Archimides principle. The applied load is due to buoyancy force and its value is 61.840 N at two planes in the z direction, and also the gravity force is 9.806 m/s² in the z direction. Fixed support is applied for this design in the +x and -x direction. The boundary condition for this design can be seen in Table 5.

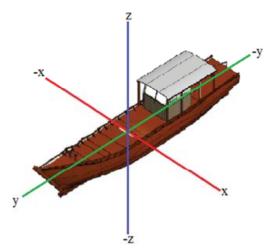


Figure 13: Axis direction to determine the boundary conditions on the connection tusks traditional ship Bagan Siapiapi

Table 5: Connection bou	Indary conditions the glue
-------------------------	----------------------------

Working Force	Axis					
Wolking Polec	Х	-X	у	-у	Z	-Z
The buoyant force	-	-	-	-	-	
Gravity force	-	-	-	-		-
Support			-	-	-	-

Bolt connection has two force direction additional worked, which bolt pretension in the y direction and -y, as shown in Table 6.

Table 6: Boundary conditions of bolt joints

Tuble of Doundary conditions of bon Jointo						
Working Force	Axis					
troning roroc	х	-X	у	-у	Z	-Z
The buoyant force	-	-	-	-	-	
Gravity force	-	-	-	-		-
Support			-	-	-	-
Bolt Pretension	-	-			-	-

As for the connected part by glue, the contact definition is frictionless with interface treatment is assumed by adjust to touch in order to define that both joints is connected without any offset. This is because it was assumed that two objects connected by glue have an coefficient of friction value approaching infinity. Besides that, the other factor involves is the selection of the type of glue such as hyper glue.

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Definition of contact in the joint is based on the friction coefficient. The value of friction coefficient is determined based on the friction between two bodies such as wood to wood or metal to metal. The values of coefficient of friction for these cases are presented in Table 7.

Material	Coefficient of Station		
Iviateriai	Friction, s		
Metal on metal	0,15 - 0,20		
Masonry on masonry	0,60 - 0,70		
Wood on wood	0,25 - 0,50		
Metal on masonry	0,30 - 0,70		
Metal on wood	0,20 - 0,60		
Rubber on concrete	0,50 - 0,90		

 Table 7: Static friction coefficient between two contact areas

3.0 RESULT AND DISCUSSION

The simulation results of the 18 models connection with a variety of materials and joining methods can be seen in Table 8.

Table 8: Von Misses equivalent tension at the connection with glue and wood screws

No	Design Connection			Maximum tension Location
		min	max	
1	LKM1	0,1795	191,14	Support
2	LKM2	0,5372	122,18	Support
3	LKM3	0,3656	170,24	Connection
4	LKM4	0,4521	188,03	Connection
5	LKK1	0,2437	126,1	Support
6	LKK2	0,5363	123,38	Support
7	LKK3	0,2966	173,1	Connection
8	LKK4	0,4762	187,86	Connection
9	BKM1	0,1322	181,37	Bolt 14 mm
10	BKM2	0,0764	222,25	Bolt 14 mm
11	BKM3	0,1547	363,36	Bolt 14 mm
12	BKM4	0,1829	338,32	Bolt 14 mm
13	BKM5	0,0454	221,79	Bolt 14 mm
14	BKK1	0,129	181,33	Bolt 14 mm
15	BKK2	0,0754	217,51	Bolt 14 mm
16	BKK3	0,155	363,36	Bolt 14 mm
17	BKK4	0,168	341,37	Bolt 14 mm
18	BKK5	0,0483	232,3	Bolt 14 mm
December	C-d- I C	Ches D	Commention Dale	

Description Code : L = Connection Glue, B = Connection Bolt, KM = Wood Meranti, KK = Wood Keruing, 1-5 = Design Connection

According to the data presented in Table 6, the best design of wooden joint to be applied based on equivalent stress is LKM2. This is because the maximum equivalent stress is 122.18 MPa, much lower than the other types of joint. The joint which has the maximum equivalent stress is BKM3. The value of its maximum equivalent stress is 363.36 MPa at 14 mm bolts. The stress contour in the joint LKM2 and BKM3 can be found in Figure 14 and Figure 15.

At the part connected by glue, the maximum equivalent stress occurs at two different places which are support area and joint area. The maximum equivalent stress for the support area occurs at the design LKM1, LKM2, LKK1 and LKK2. As for the joint area, the maximum equivalent stress occurs at the design LKM3, LKM4, LKK3 and LKK4. For the connected part by bolts, the maximum equivalent stress occurs at the 14 mm bolts for all designs.

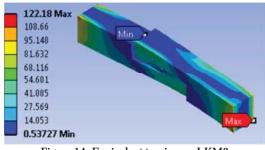


Figure 14: Equivalent tension on LKM2

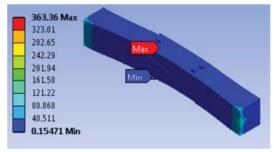


Figure 15: Equivalent tension on BKM3

3.2 Total Deformation

Besides the equivalent stress, the deformation in the wooden joint is also important to be considered in the selection of wooden joint design. Simulation results calculate the deformation for 18 joint designs and its value can be seen in Table 9.

No	Design Connection	Deformation (mm)
1	LKM1	24,386
2	LKM2	27,586
3	LKM3	21,293
4	LKM4	21,457
5	LKK1	24,208
6	LKK2	27,179
7	LKK3	20,905
8	LKK4	21,133
9	BKM1	1,635
10	BKM2	1,694
11	BKM3	1,487
12	BKM4	1,6091
13	BKM5	1,5921
14	BKK1	1,521
15	BKK2	1,576
16	BKK3	1,487
17	BKK4	1,4979
18	BKK5	1,4829

Description Code : L = Connection Glue, B = Connection Bolt,

KM = Wood Meranti, KK = Wood Keruing, 1-5 = Design Connection

^{3.1} Equivalent Von-Misses Stress

Based on the simulation results using the finite eglueent method (Table 8 and 9), it showed that the highest stress at the joint occur at the joint No. B3 (oblique lip joint with bolt) for both meranti and keruing. The value of stress for this type of joint is 363.36 MPa. The design which produces the smallest stress is the safest one and it is obtained by design No. L2 (hook lip joint) which use the meranti wood materials. The value of stress for this type of joint is 122.18 MPa. If the design is evaluated based on the deformation, thus the design No. L2 (hook lip joint) which use meranti wood materials produces the deformation around 27.586 mm, be seen in Figure 16. The smallest deformation is occur at the design No. B5 which use keruing wood materials. The design can be seen in Figure 17. The datail for equivalent stress and total deformation for the safest and best design are presented in Figure 18 and 19.

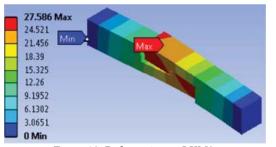


Figure 16: Deformation on LKM2

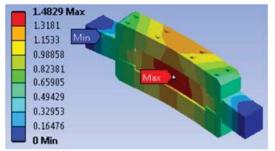
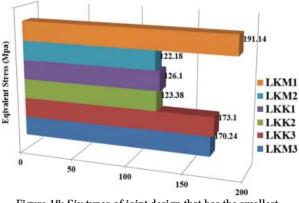
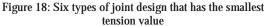
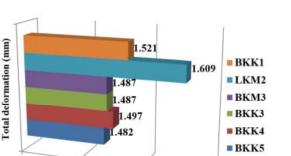


Figure 17: Deformation on BKK5







1.650 Figure 19: Six types of connections with joint design with the smallest deformation value

1.550

4.0 CONCLUSION

1.350

1.450

The study conducted in this numerical simulation produces 18 simulation models. These models are then used to study the strength of the wooden joint in the traditional wooden ship structure. It can be concluded that:

- The design of joints No.1 (L1/B1) produces a relative small stress compare to the other design of joints.
- In general, the use of glue in the joint parts produces a smaller stress; however it is heavily depends on the type of the glue itself.
- Both of wooden materials meranti and keruing have a relatively similar performance subjected to applied loads in wooden ship structure.

It is suggested that the results from simulations needs a validation experimentally.

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